



Thermal-Hydraulic Modeling of the iPWR SMR Using RELAP5-3D

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Outline



- ❑ Introduction
- ❑ Development Process
- ❑ iPWR RELAP5-3D model
- ❑ Steady-State Results
- ❑ Transient (Turbine Trip)
- ❑ Future work

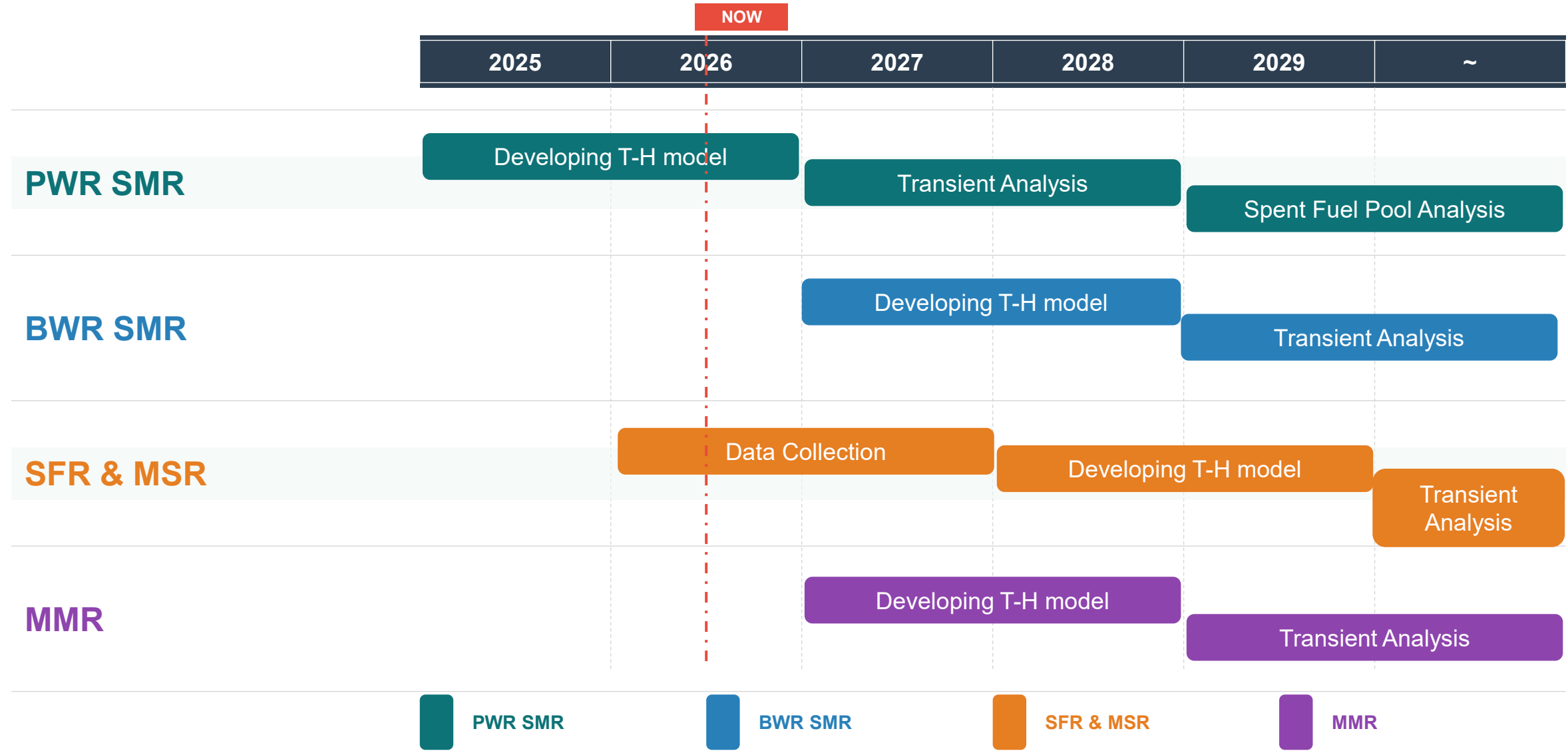


Introduction-NARI SMR

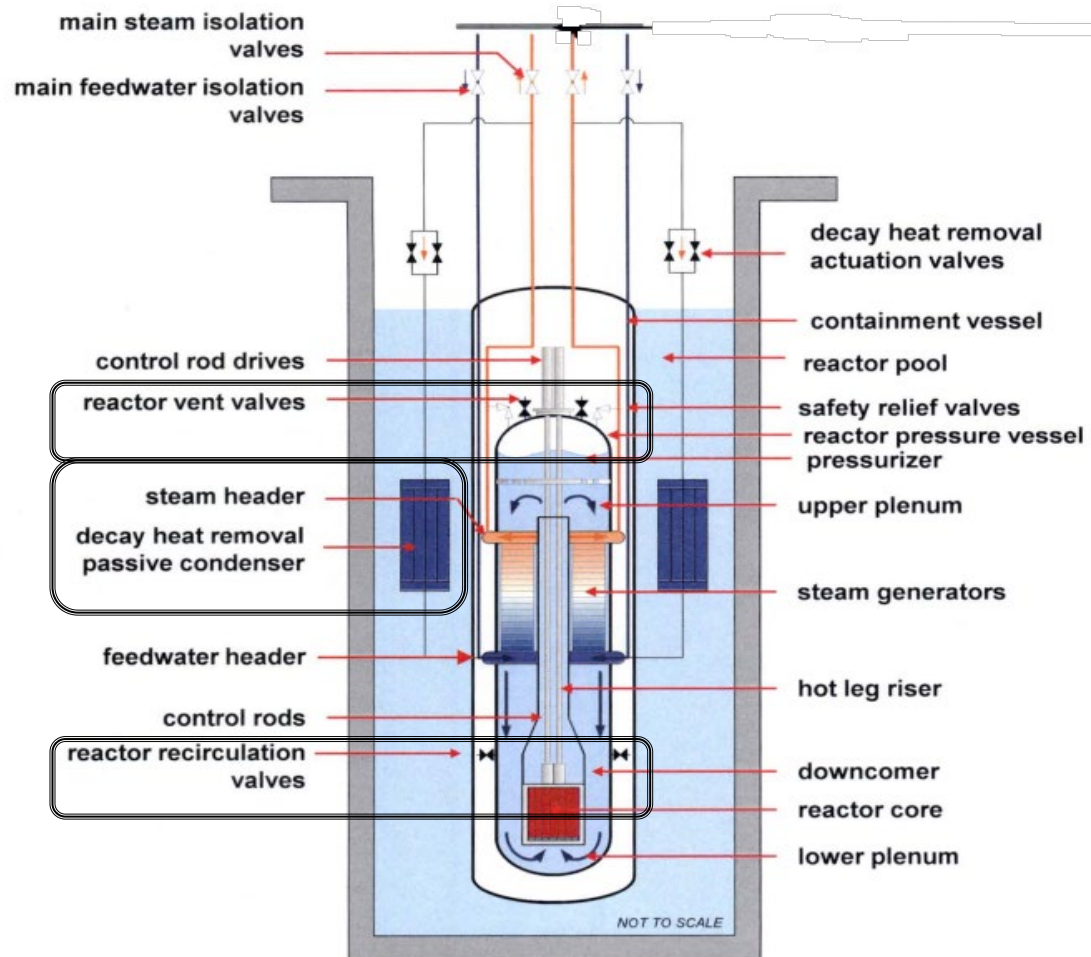
Research on Small Modular Reactors

- 1. Reactor Operating Safety Analysis**
- 2. Probability Risk Assessment**
- 3. Radioactive Waste Management and Emergency Planning Zone**
- 4. Fuel Materials, Seismic Structure and Digital Control**
- 5. Offshore Advanced Reactors, Reactor Technical Assessment, Economic Analysis, Public Communication and Regulatory Study**

Introduction-NARI SMR



Introduction-iPWR

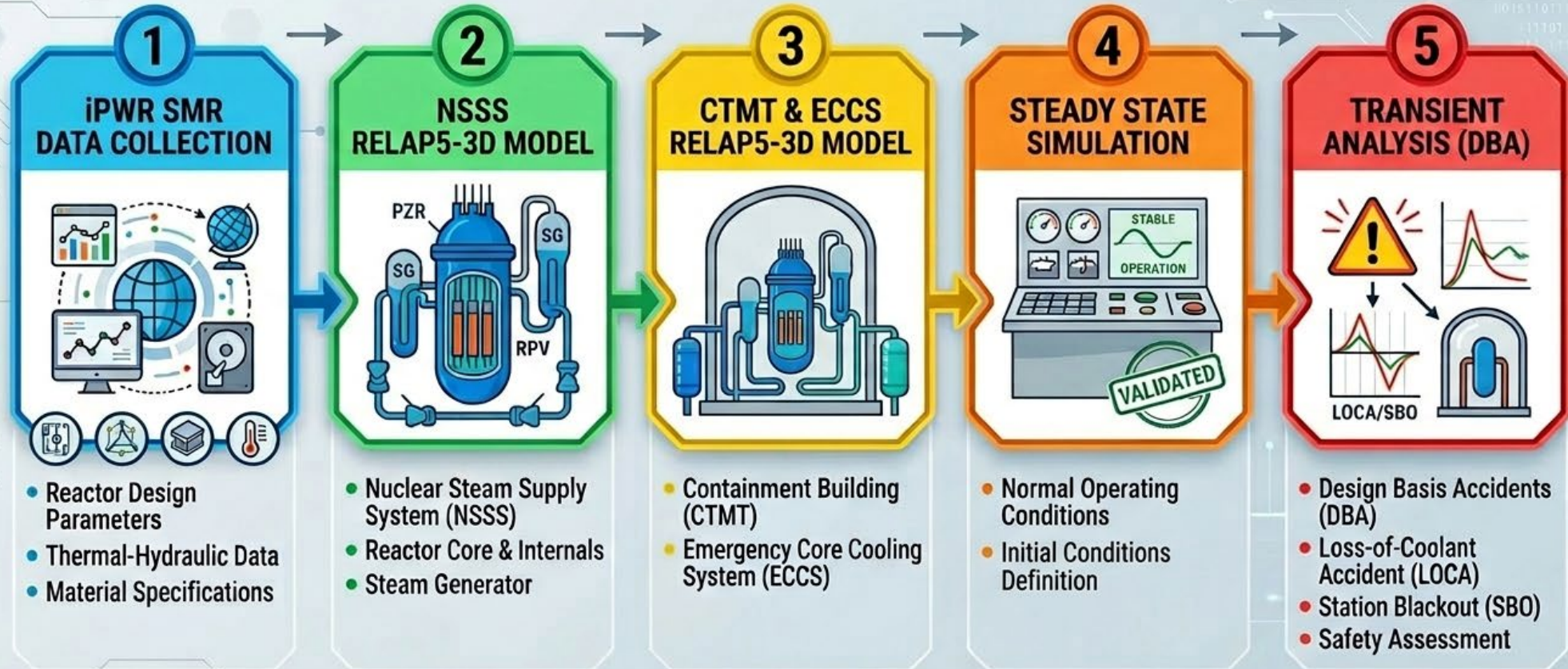


NuScale SMR module

- ❑ Integral Reactor Design
- ❑ No RCP->Natural Circulation
- ❑ HCSG
- ❑ Passive Safety system-> DHRS
- ❑ ECCS-> RVV & RRV

Development Process

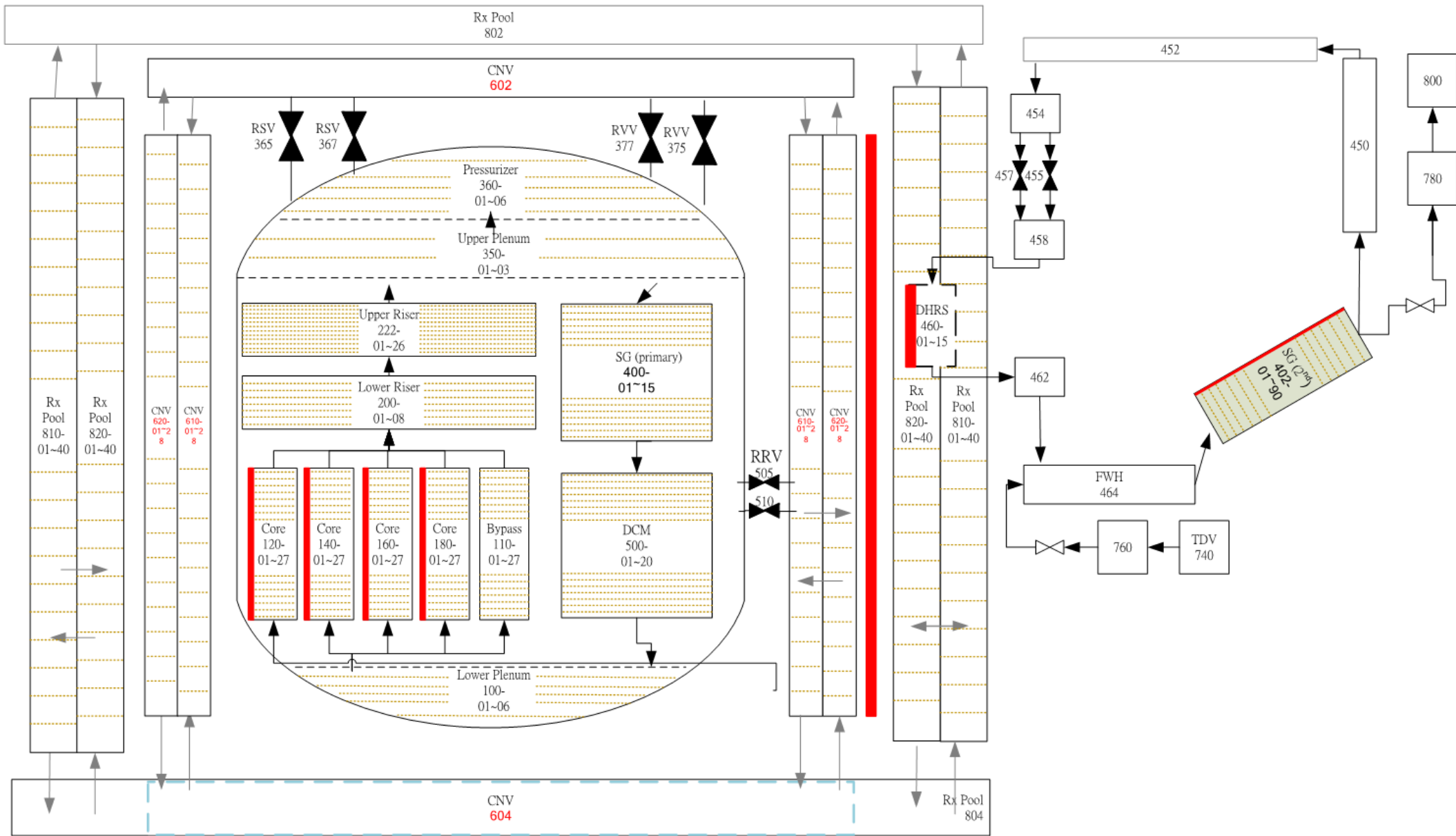
iPWR SMR DEVELOPMENT AND SAFETY ANALYSIS WORKFLOW



PROCESS BASED ON RELAP5-3D SIMULATION



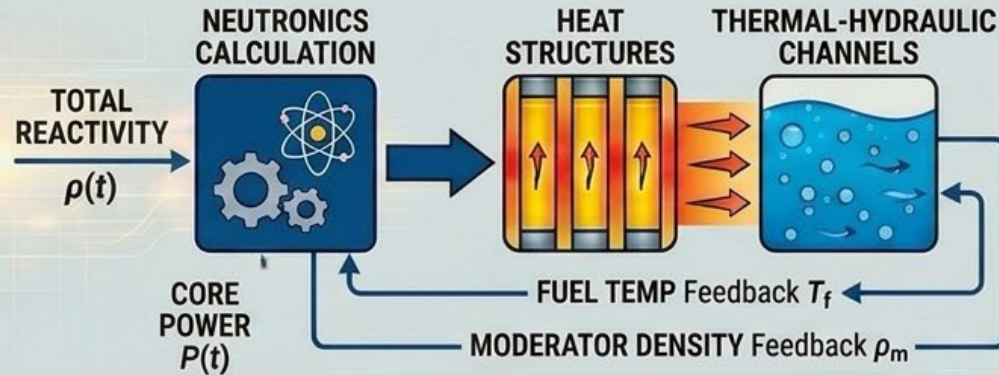
iPWR RELAP5-3D model



iPWR RELAP5-3D model

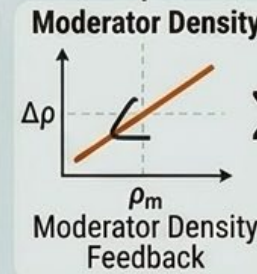
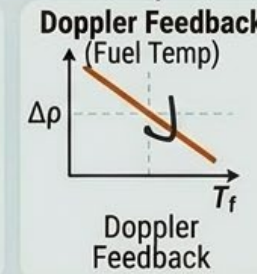
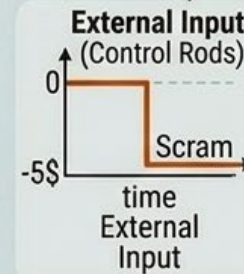
VISUALIZING RELAP5-3D POINT KINETICS MODEL

1. COUPLING ARCHITECTURE



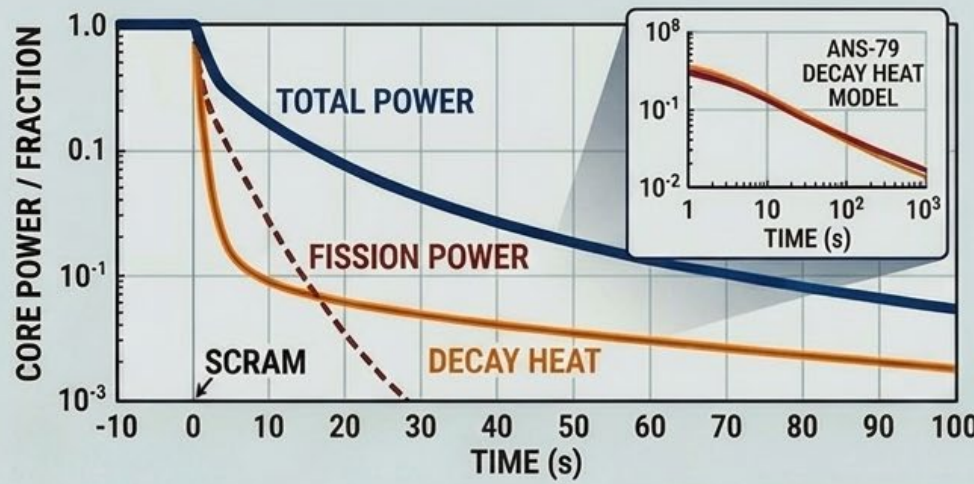
2. REACTIVITY FEEDBACK COMPONENTS

$$\rho(t) = \rho_{\text{ext}}(t) + \Delta\rho_{\text{fuel}}(T_f) + \Delta\rho_{\text{mod}}(\rho_m)$$



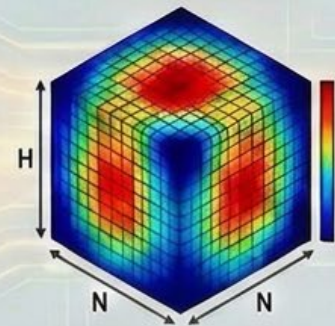
$\sum P_{\text{feedback}}$

3. POWER TRANSIENT CURVE

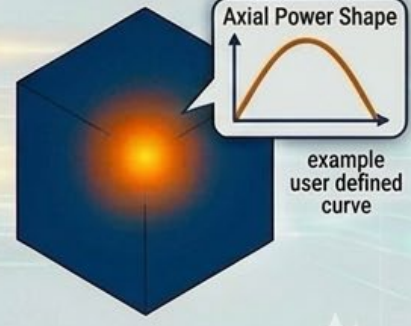


4. GEOMETRIC SIMPLIFICATION

3D SPATIAL KINETICS



POINT KINETICS



SAVES COMPUTATION TIME FOR DBA ANALYSIS



iPWR RELAP5-3D model



Doppler feedback

1. Establish the power table steady state.

2. Get the htvat (T_{f0})

3. Assume $FTC = -0.0021 \text{ } \$/^{\circ}\text{F}$,
$$R = FTC \times (T_f - T_{f0})$$

4. Generate the Doppler Reactivity Table(300006XX)

5. Get the s.s. fuel temperature from output, replace the data into kinetics model deck.

* fuel temperature(F)		reactivity
30000601	100.0	1.50465
30000602	500.0	0.66465
30000603	816.5	0
30000604	1000.0	-0.38535
30000605	...	...
30000606	...	...
30000607	...	...
30000608	...	...
30000609	...	...

0	At time=	1500.00	sec	str.no.	mesh point temperatures	Sum of the (degF)
4000-001	429.05	460.75				
4000-002	435.77	463.22				
4000-003	442.06	465.55				
4000-004	447.81	467.67				
4000-005	452.77	469.52				
4000-006	457.08	471.13				
4000-007	475.54	490.19				
4000-008	479.37	491.62				
4000-009	482.60	492.83				
4000-010	485.28	493.84				
4000-011	487.52	494.68				
4000-012	489.28	495.34				
4000-013	495.95	503.23				



iPWR RELAP5-3D model



Moderator feedback

$$MDC = MTC / \left(\frac{\partial \rho}{\partial T}\right)_P$$

$$\left(\frac{\partial \rho}{\partial T}\right)_P$$

(1) At Pressure=2000 psia · calculate the $(\partial \rho / \partial T)$ under different fluid temperature

(2) Correlation :

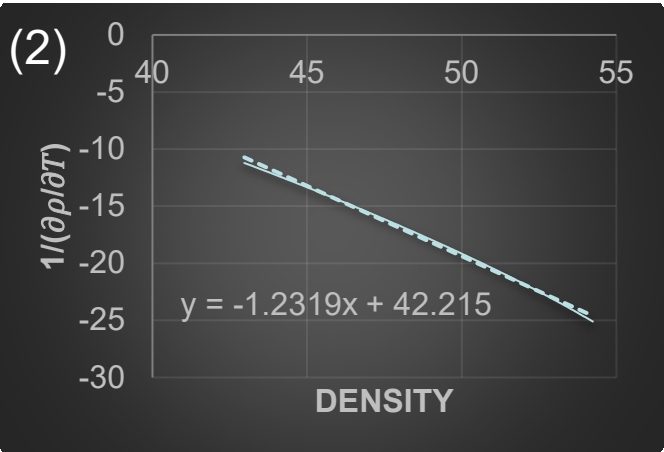
$1 / \left(\frac{\partial \rho}{\partial T}\right)_P$ v.s. density

$$\frac{1}{\left(\frac{\partial \rho}{\partial T}\right)_P} = -1.2319\rho + 42.215$$

(3) MDC

Assume $MTC = -0.01 \text{ } \$ / ^\circ\text{F}$,
 $R = 0.0061595\rho^2 - 0.42215\rho + 6.1823$

(1) T(F)	density@2000psia(lbm/ft3)	drdt(lbm/ft3*F)	1/drdt(ft3*F/lbm)
599	42.97	-0.08917	-11.21463
590	43.75	-0.08324	-12.01351
580	44.55	-0.07776	-12.86027
570	45.3	-0.07314	-13.67151
560	46.02	-0.06919	-14.45287
...	...	...	...
...	...	...	...
...	...	...	...



*(3)	Density(lbm/ft3)	Reactivity(dollars)
30000501	37.1	-1.00148
30000502	45.53	-0.26968
30000503	45.83	-0.22750
30000504...	...	...
30000505...	...	...
30000506...	...	...



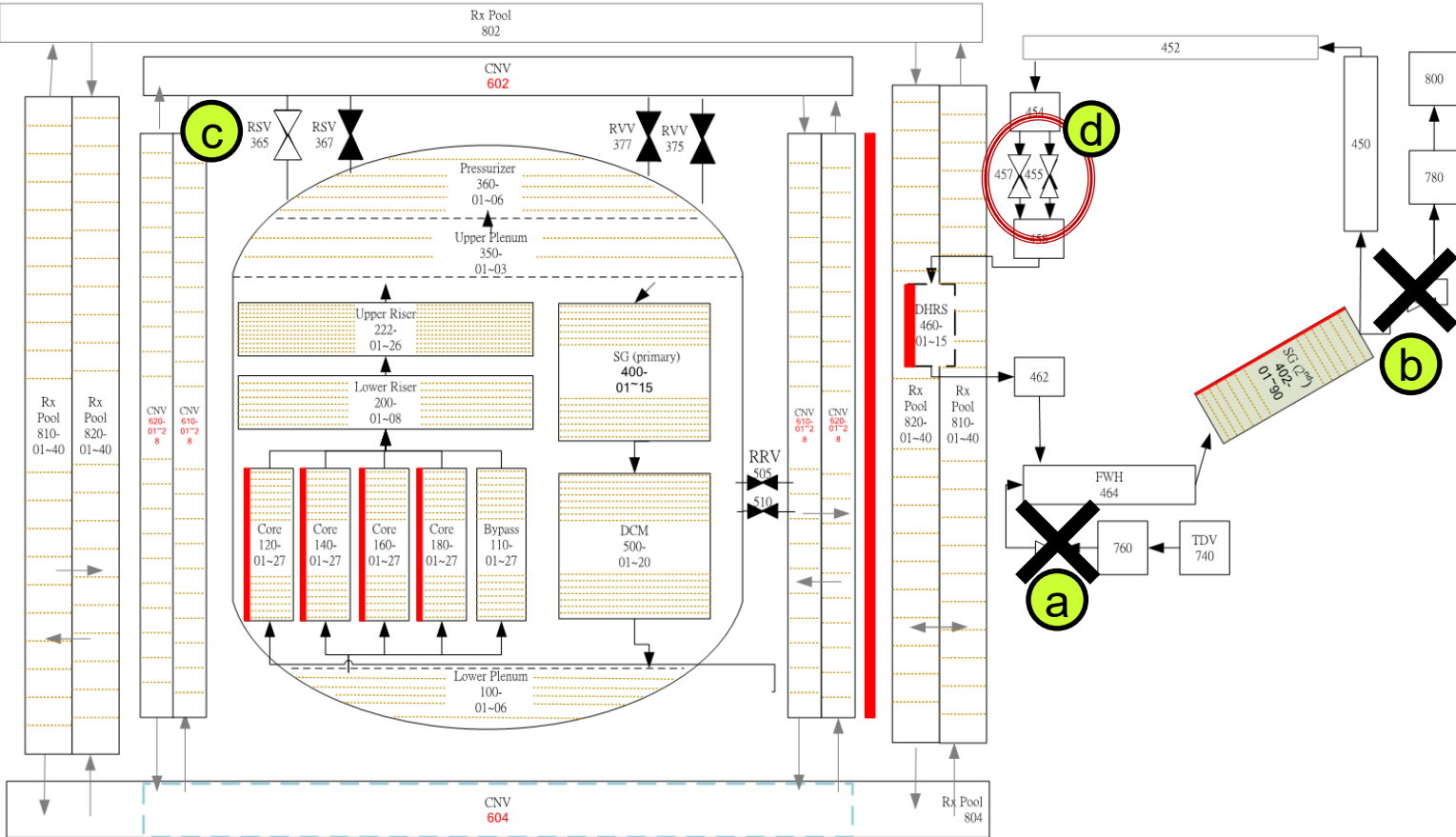
Steady-State Results



Parameters	FSAR	RELAP5-3D	Differ.(%)
Thermal power (MW)	250.0	250.0	0.0
Primary-side mass flow (lbm/s)	1616.7	1622.9	0.4
Primary-side pressure (psia)	2000.1	1996.7	-0.2
Core inlet temperature (°F)	481.0	479.8	-0.2
Core average temperature (°F)	540.0	538.5	-0.3
Core outlet temperature (°F)	599.0	597.3	-0.3
PZR water level (%)	60.0	59.7	-0.5
Secondary-side mass flow (lbm/s)	226.6	226.6	0.0
SG outlet pressure (psia)	475.0	475.5	0.1
SG inlet temperature (°F)	250.0	250.1	0.0
SG outlet temperature (°F)	536.0	545.0	1.7
Core bypass flow (%)	7.5	7.4	-1.6



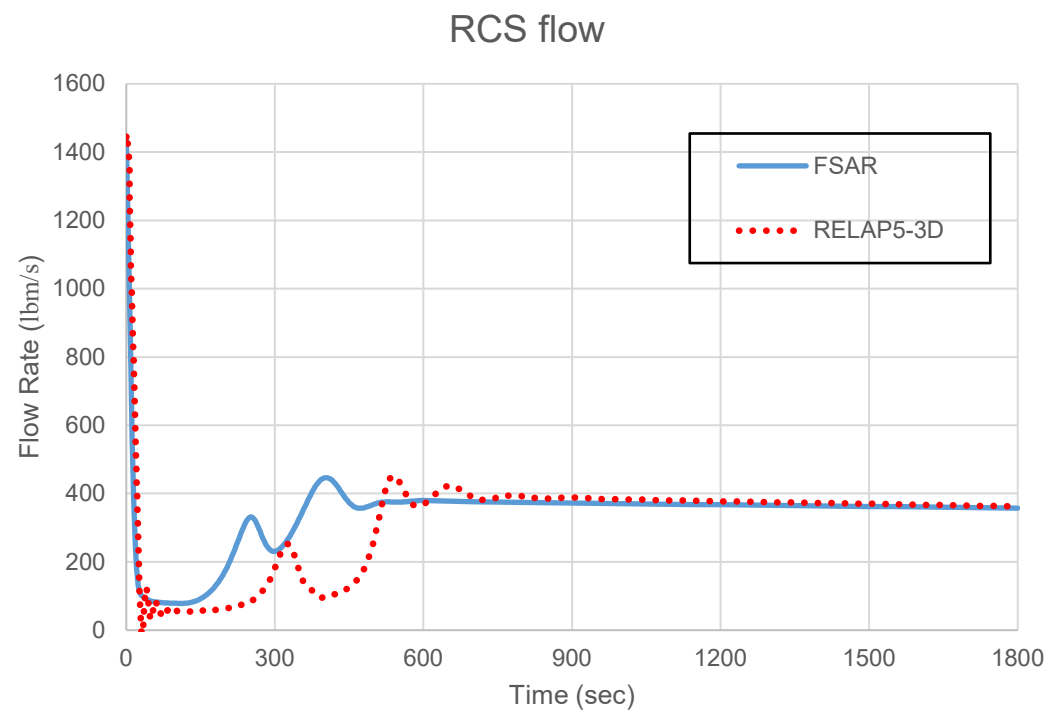
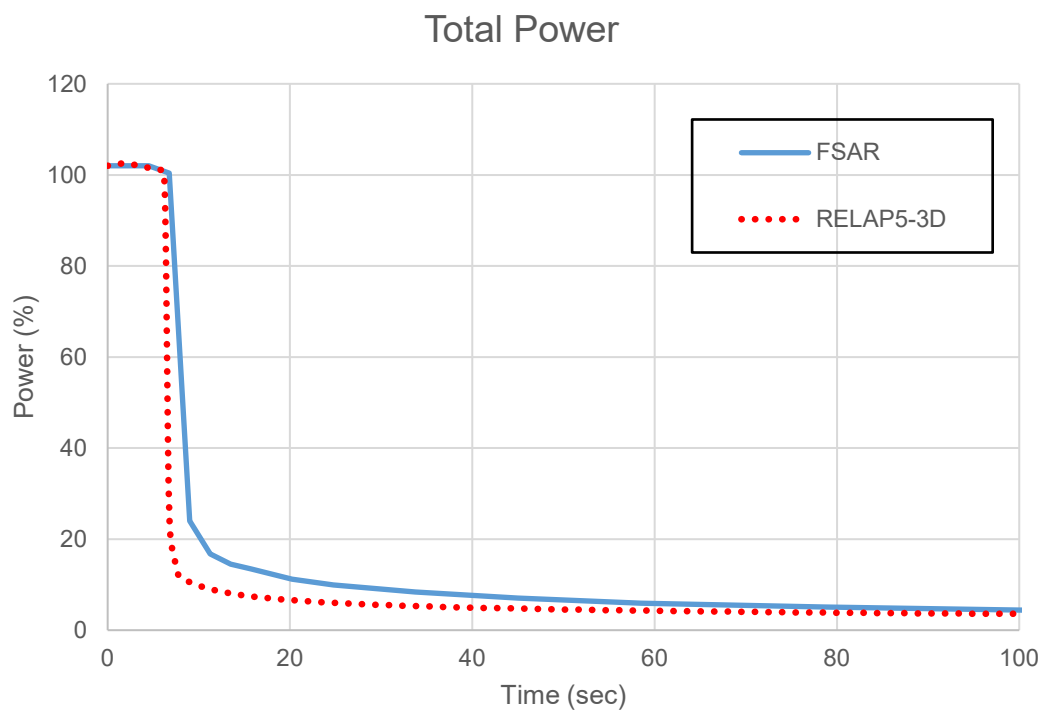
Transient (Turbine Trip)



Sequence of Event	Time(s) FSAR	Time(s) RELAP
(a) Event initiator - TT and loss of FW flow due to assumed LOOP	0	0
(b) Turbine stop valves fully closed (assumption)	0	0
Reactor trip, SSI and DHRS actuation, PZR heater trip (high PZR pressure 2100 psia)	7	6(4+2)
(c) RSV lifts	8	NA
Peak RCS pressure	9	7
(d) DHRS actuation valves full open	37	36

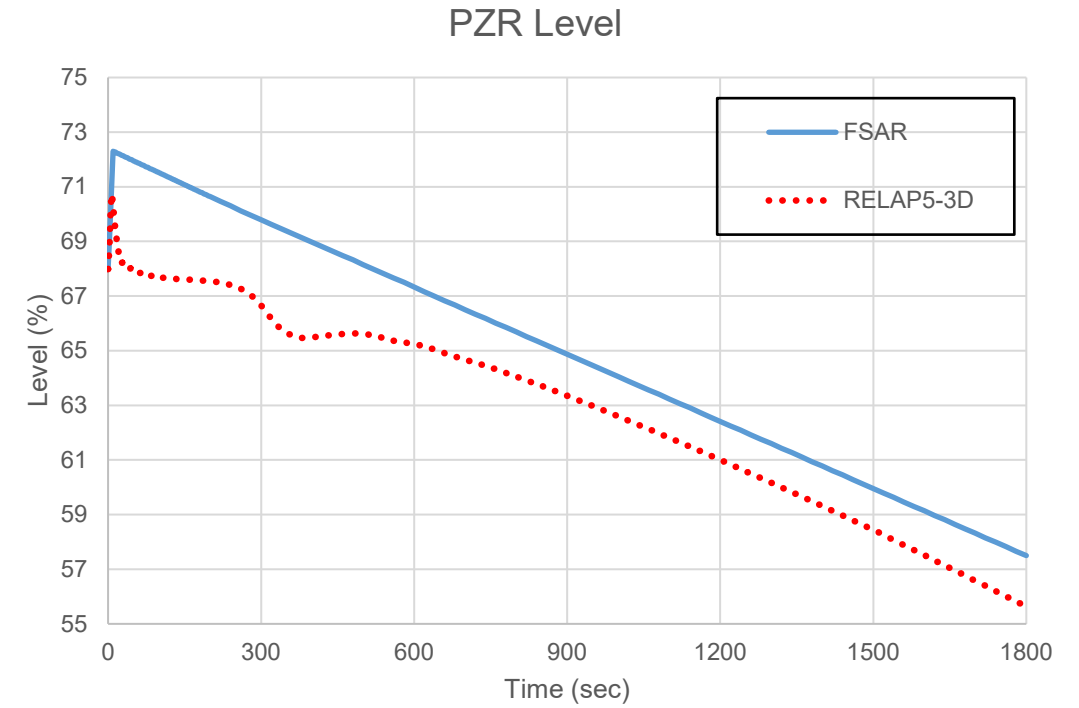
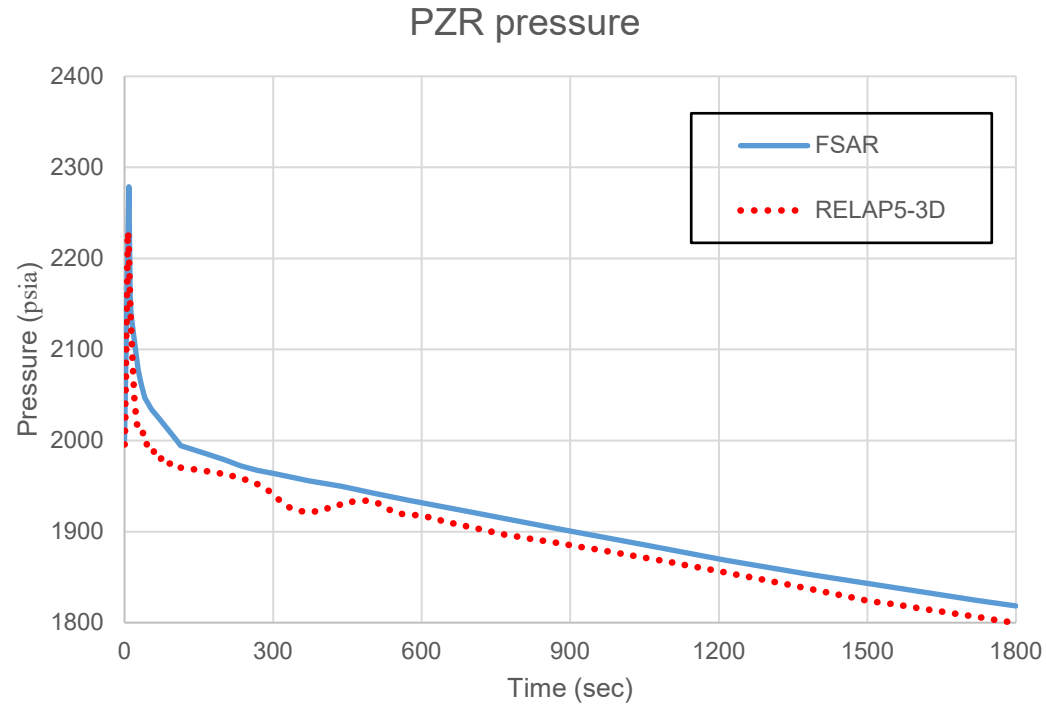


Transient (Turbine Trip)





Transient (Turbine Trip)

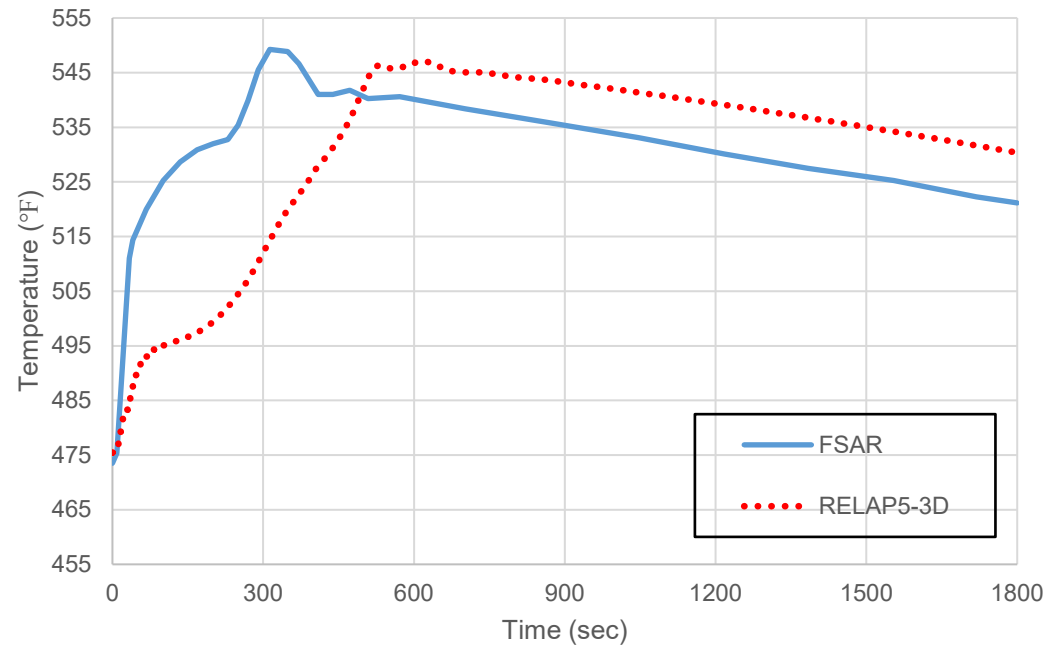


Lower power -> lower pressure-> lower water level

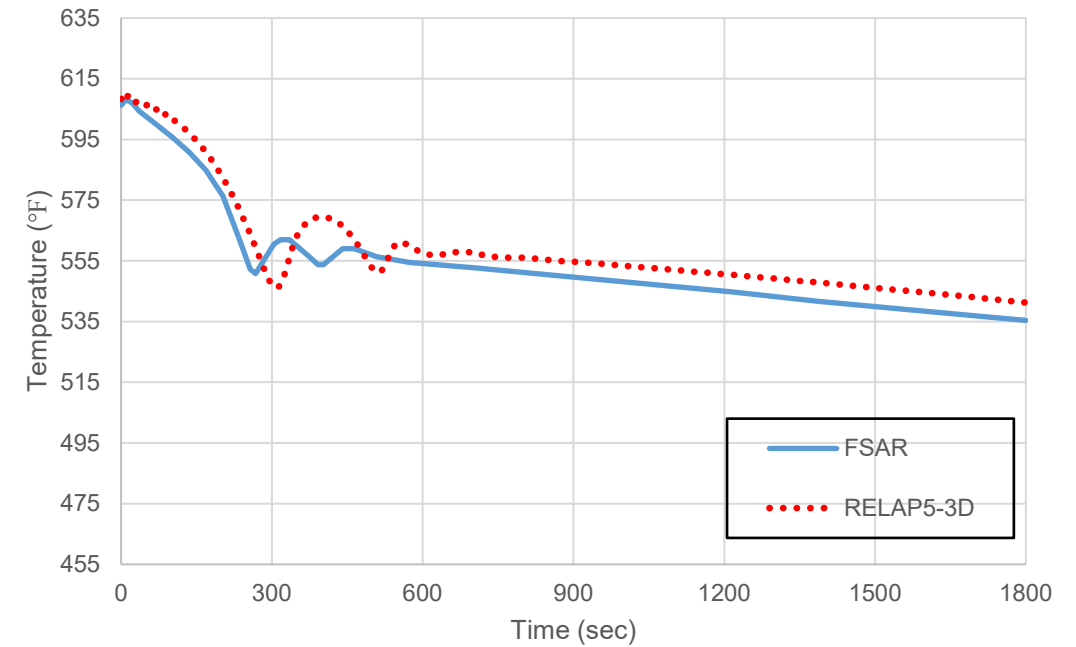


Transient (Turbine Trip)

RCS cold T



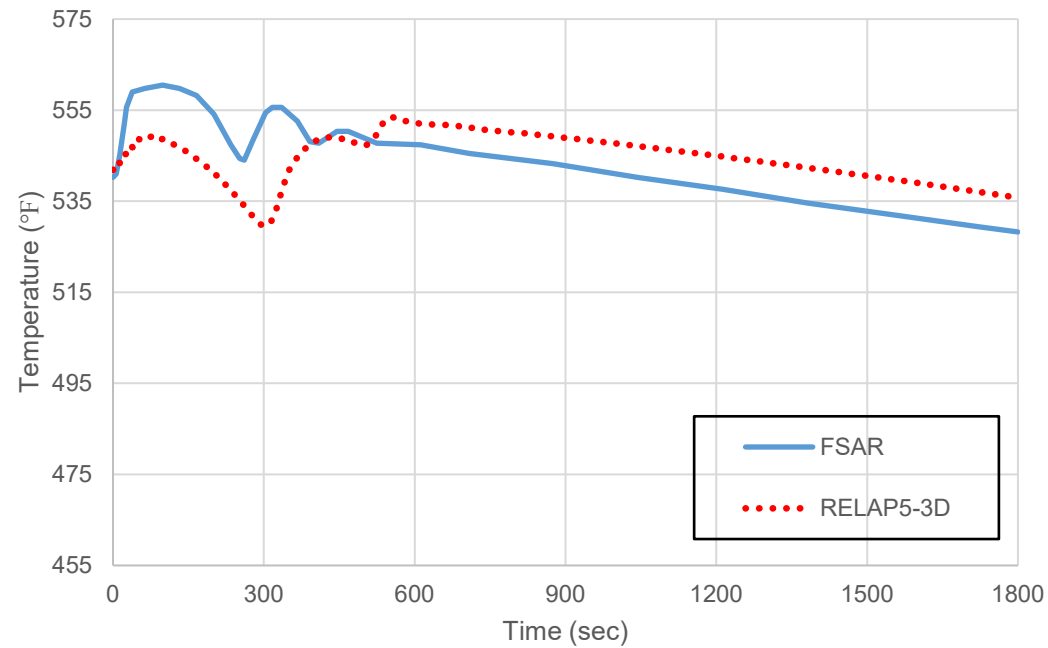
RCS hot T



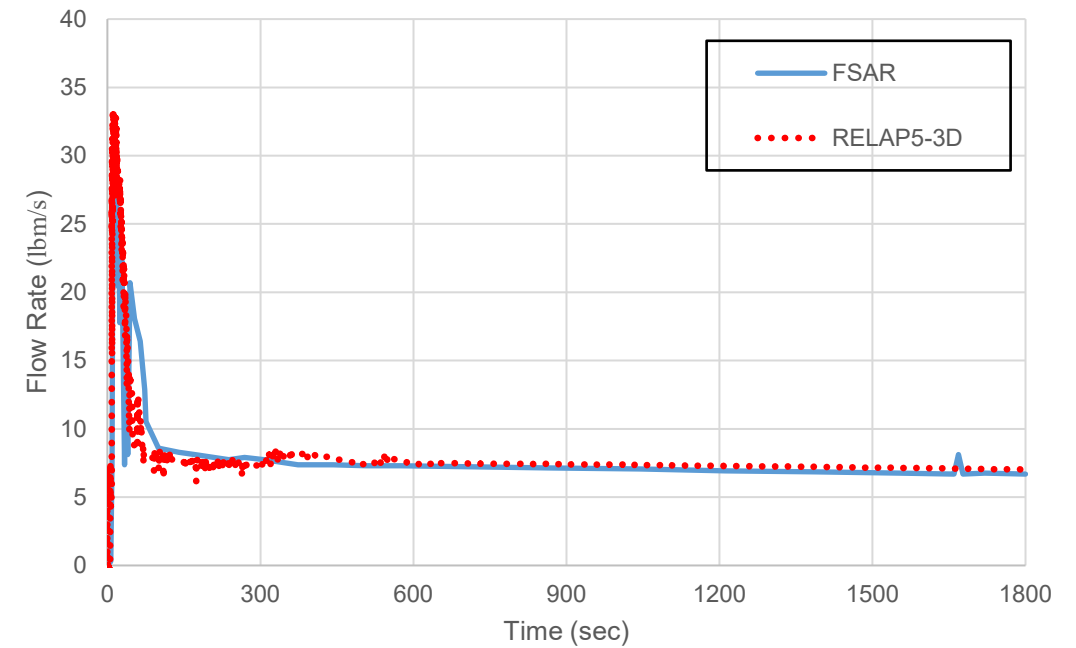


Transient (Turbine Trip)

RCS avg. T



DHRS outlet flow





Transient (Turbine Trip)



□ Result discussions:

- Lack of the exact “SCRAM curve ” for the safety analysis.
- FSAR using NRELAP5 which has “HCSG” model.
- This case can benchmark the DHRS flow.



Future Work

- ❑ Sensitivity Analysis, ex: **nodalization** refinement ,
scram delay time
- ❑ Extension of transient behavior, including **LOCA**,
SBO, etc.
- ❑ Combined with **VIPRE** to calculate **MCHFR**.
- ❑ Other types of SMR.



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National Atomic Research Institute

Thank You for Your Attention

>>> Q&A



Reference



- NuScale Power, LLC, "Standard Design Approval Application, Part 2 – Final Safety Analysis Report," SDA-101, Rev. 1, Nov. 2022. [Online]. Available: NRC ADAMS Accession No. ML22365A006.
- P. Freitag, "Transient Thermal-hydraulic Simulation of a Small Modular Reactor in RELAP 5," M.S. thesis, Dept. of Mechanical, Industrial and Systems Engineering, University of Rhode Island, 2018.
- K. Skolik, C. Allison, J. Hohorst, M. Malicki, M. Perez-Ferragut, L. Pieńkowski, and A. Trivedi, "Analysis of loss of coolant accident without ECCS and DHRs in an integral pressurized water reactor using RELAP/SCDAPSIM," *Progress in Nuclear Energy*, vol. 134, Art. no. 103648, 2021, doi: 10.1016/j.pnucene.2021.103648