

# ***Validation of a Detailed RELAP5-3D Point Kinetics Model of TREAT***

**C. B. Davis**

2018 IRUG Meeting

Idaho Falls, ID

April 30 – May 4, 2018

[www.inl.gov](http://www.inl.gov)



# Outline

- Background
- Description of TREAT
- Description of the detailed RELAP5-3D model
- Validation results
- Conclusions

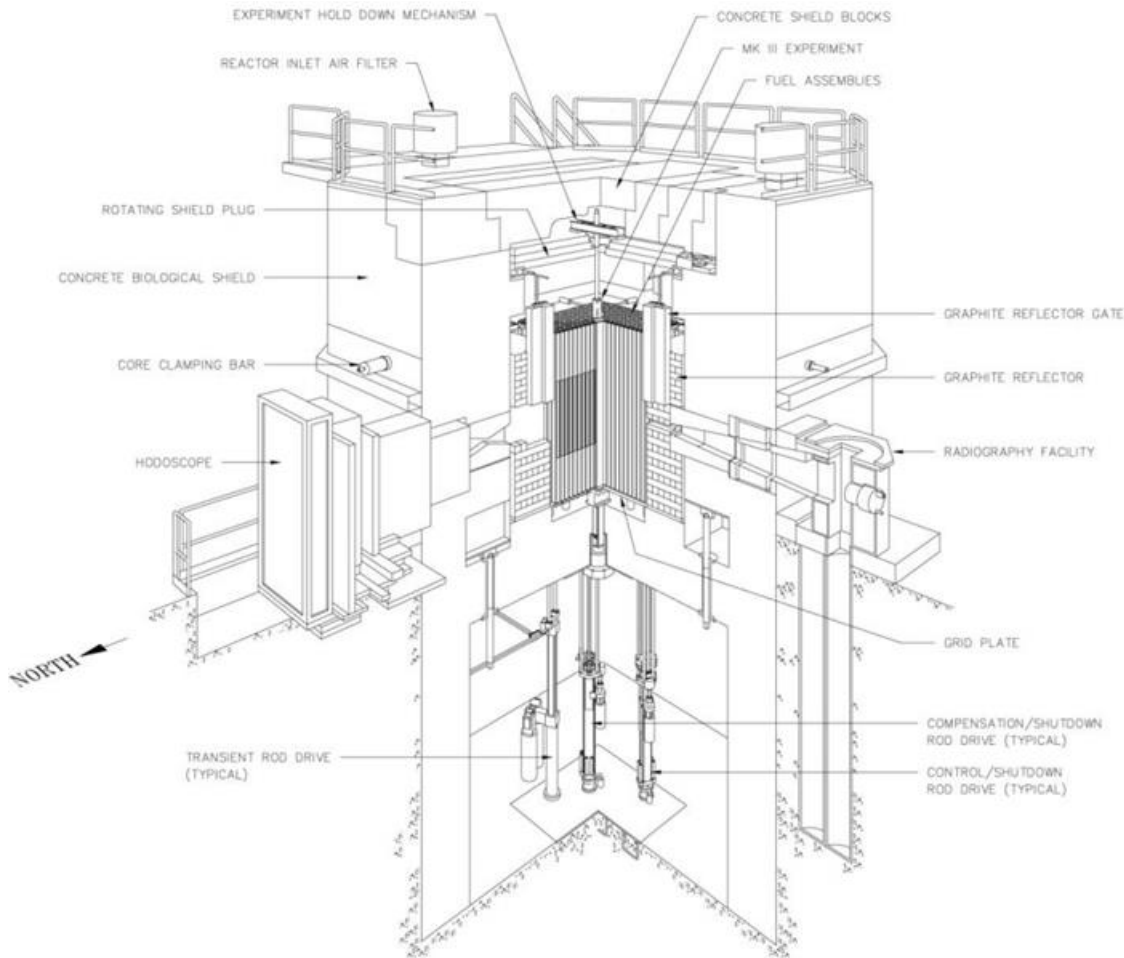
## Background

- The Transient Reactor Test (TREAT) facility has been restarted to test accident tolerant fuels for light water reactors that are designed to have better performance than traditional Zircaloy-clad  $\text{UO}_2$  fuel during normal operation and accidents
- New experiments will be performed in the next few years to test proposed fuel concepts and provide data for assessment of advanced multi-physics computer codes
- Calculations are required now to demonstrate that the experiments will meet program objectives and can be performed safely
  - The advanced multi-physics computer codes are not ready yet
  - The safety calculations for the first experiments will be performed with RELAP5-3D
- A simple RELAP5-3D point kinetics model of TREAT was developed and validated previously as described at the 2015 IRUG meeting
- A more detailed RELAP5-3D model is the subject of this presentation

## ***Description of TREAT***

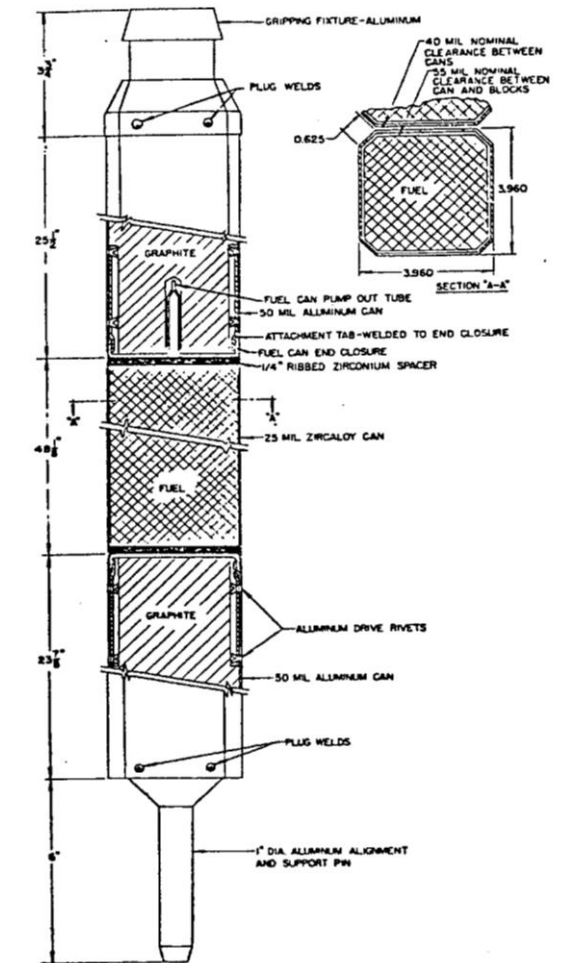
- TREAT is a dry reactor that went critical in 1959
- Operations were suspended in 1994
- The reactor was restarted this fiscal year
- Driver core is made up of uranium dispersed in graphite blocks encapsulated by Zircaloy cans
- Square layout with 361 positions that are filled with fuel or dummy assemblies
- The size of the core varies from small to large (~ 150 to 340 fuel assemblies)
- Dummy assemblies are located around the periphery of the core and are filled with graphite for additional reflection
- Experiments are placed in the center of the core

# Description of TREAT (cont'd)



- Core is set on a square gridplate
- Core is surrounded by graphite reflectors
- A small amount of cooling is provided by downflow of air
- The heat capacity of the graphite provides the primary heat sink during transients
- Reactivity control provided by three banks of control rods

# Description of TREAT fuel assembly



- Each fuel assembly is a 4x4” “square” that contains fuel, a gas gap, and a Zircaloy can
- The gas gap was evacuated during manufacture
- Active core is 48” tall
- There is a small gap between fuel elements for air flow
- More that 50% of the flow area is located near the corners, while the wetted perimeter of the corners is less than 20% of the total

## *Description of TREAT (cont'd)*

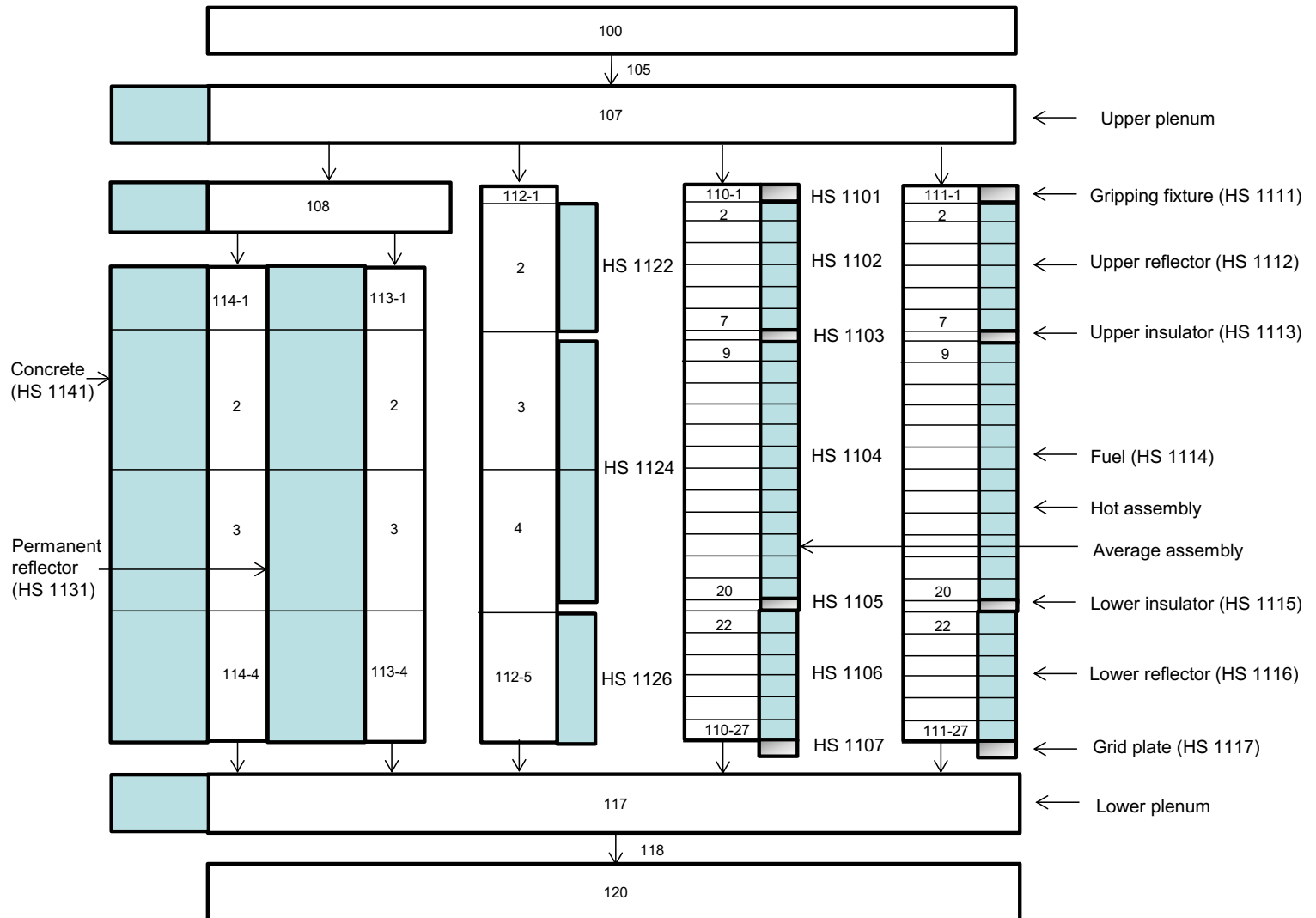
- TREAT can perform two types of transients
  - Unshaped transients
    - The only reactivity addition is that required to initiate the experiment
    - The reactor power responds naturally due to thermal feedback
  - Shaped transients
    - The transient rods are moved during the test to obtain a desired power curve
    - The reactor power responds to the rod movement and the thermal feedback

## ***Description of the detailed RELAP5-3D model***

- The detailed RELAP5-3D model was developed to calculate the reactor response during experiments and accidents
- The model represents hot and average fuel assemblies, the reflectors, and the concrete
- The model accounts for
  - Reactivity feedback
  - Axial conduction in the fuel elements using a conduction enclosure model
  - Forced convection cooling due to blower operation
  - Natural convection cooling in the event of blower failure
- The model monitors oxidation of the Zircaloy can at the peak power location in the hot fuel assembly



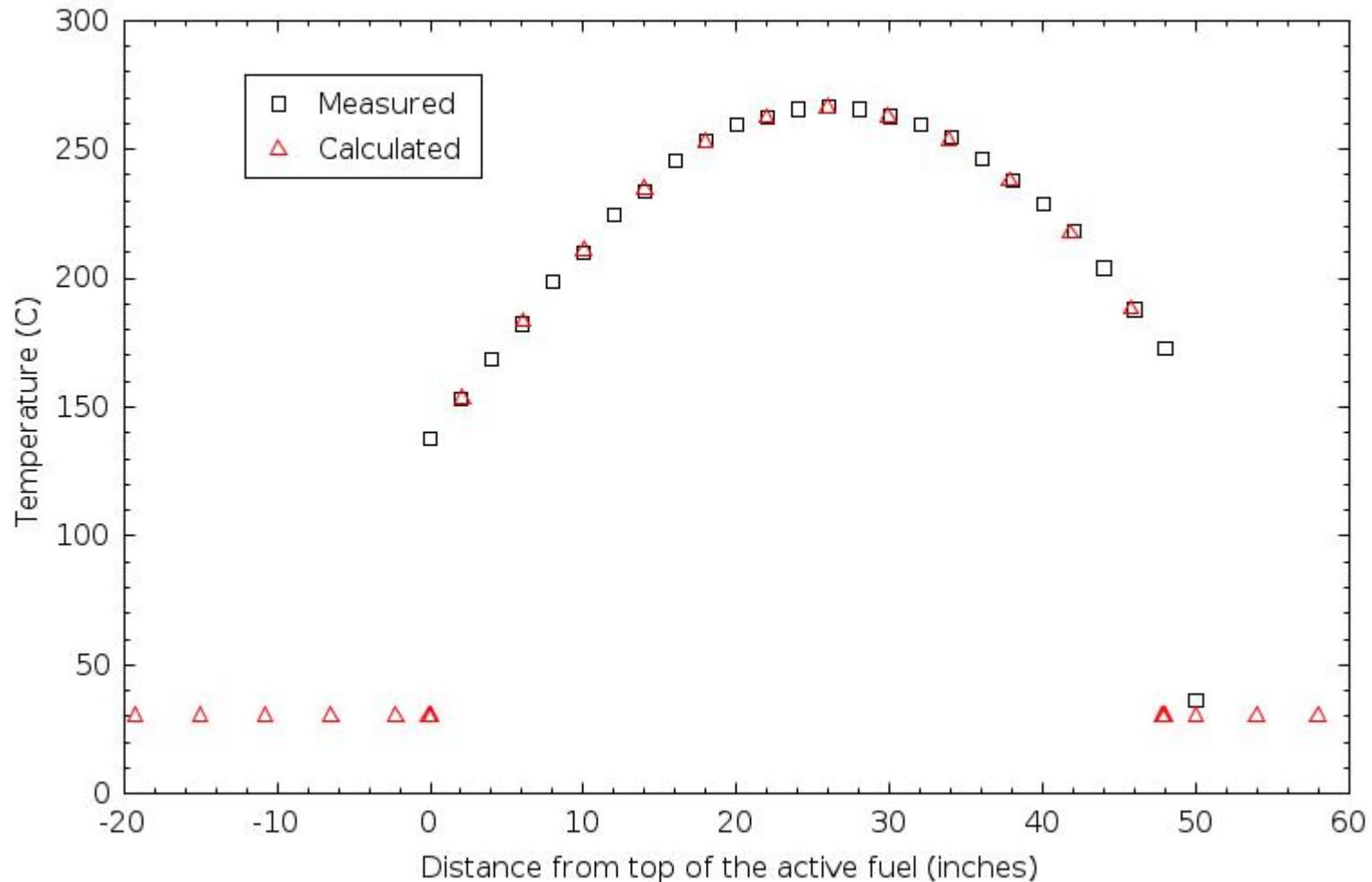
# Description of the RELAP5-3D model (cont'd)



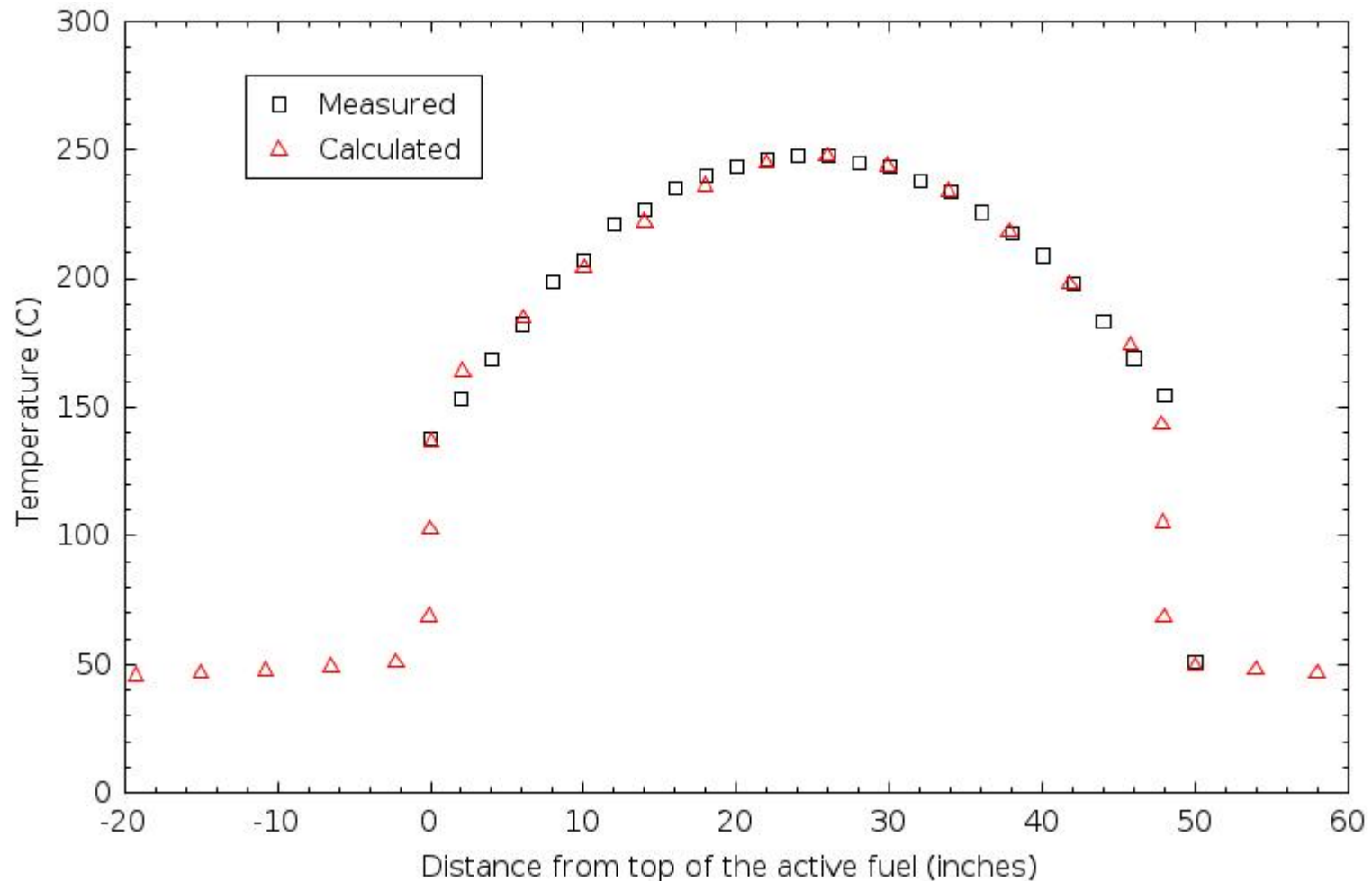
## ***Validation results were generated for a historical cooldown test***

- Test initiated by an unshaped reactivity transient that established the initial axial temperature distribution
  - Axial conduction was the dominant heat transfer mechanism prior to 87 minutes, when the blowers were turned on
  - Forced convection to air was the dominant heat transfer mechanism after 87 minutes
- The model was adjusted to match temperature measurements
  - The axial thermal conductivity of the fuel was reduced from a nominal value of 21 W/m-K to 13 W/m-K
  - The axial thermal conductivity of the insulators was set at 0.15 W/m-K
  - The heat transfer coefficients were multiplied by a fouling factor of 0.45
    - Most of the heat transfer area is cooled by a relatively small fraction of the flow that probably sees much worse than average heat transfer conditions

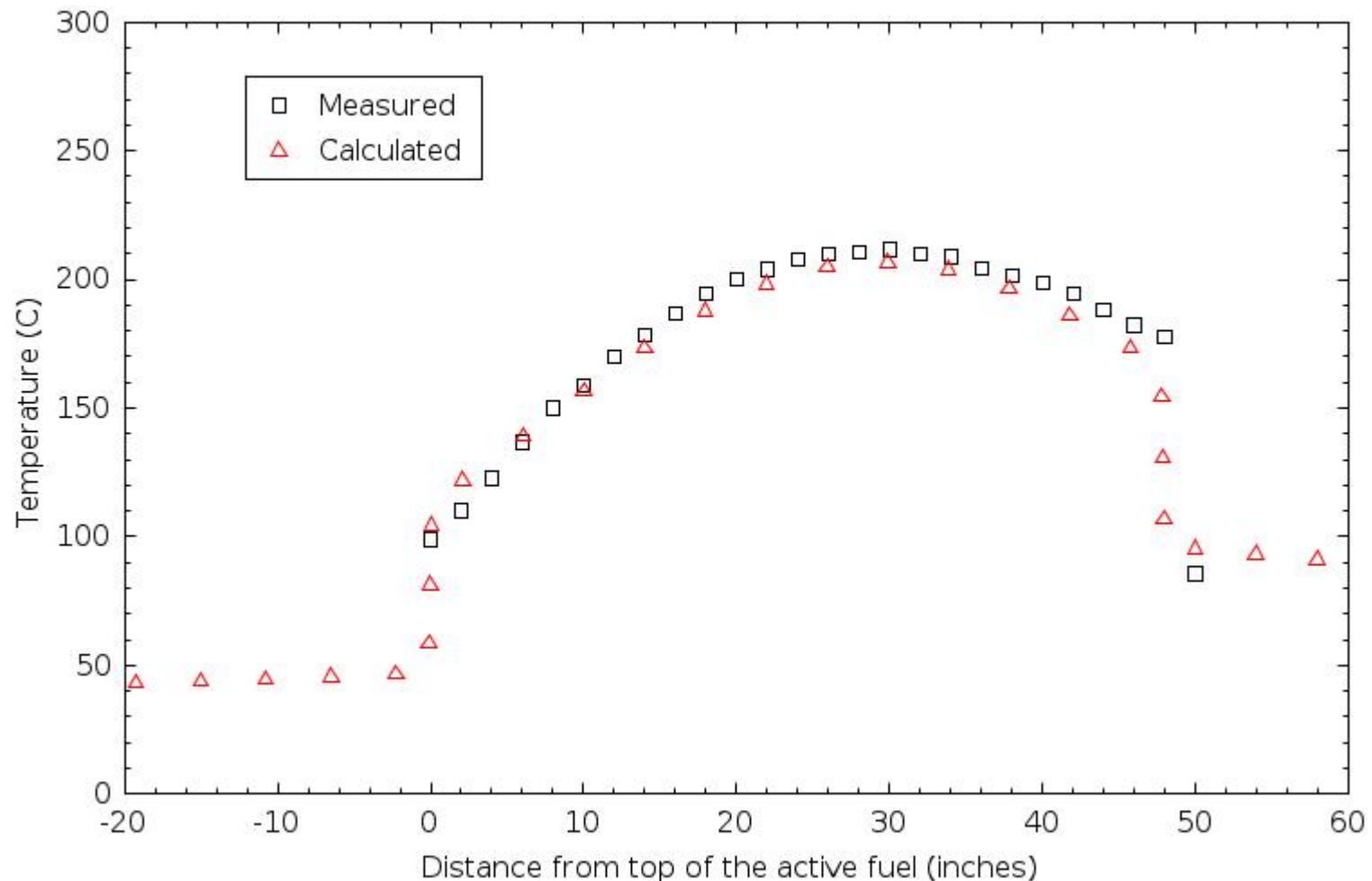
# Axial temperature profiles in the historical cooldown test at 0 min



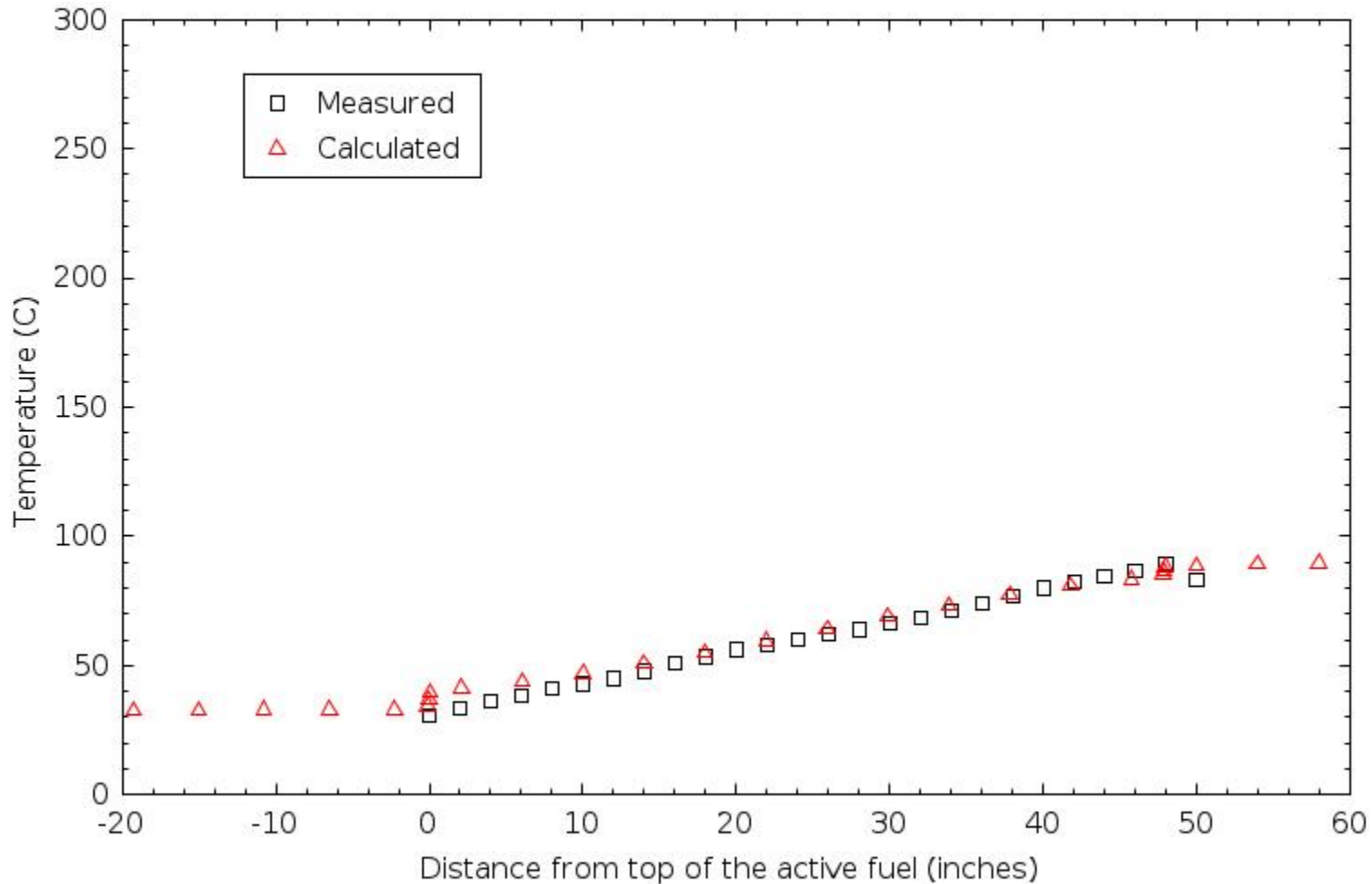
# Axial temperature profiles in the historical cooldown test at 85 min



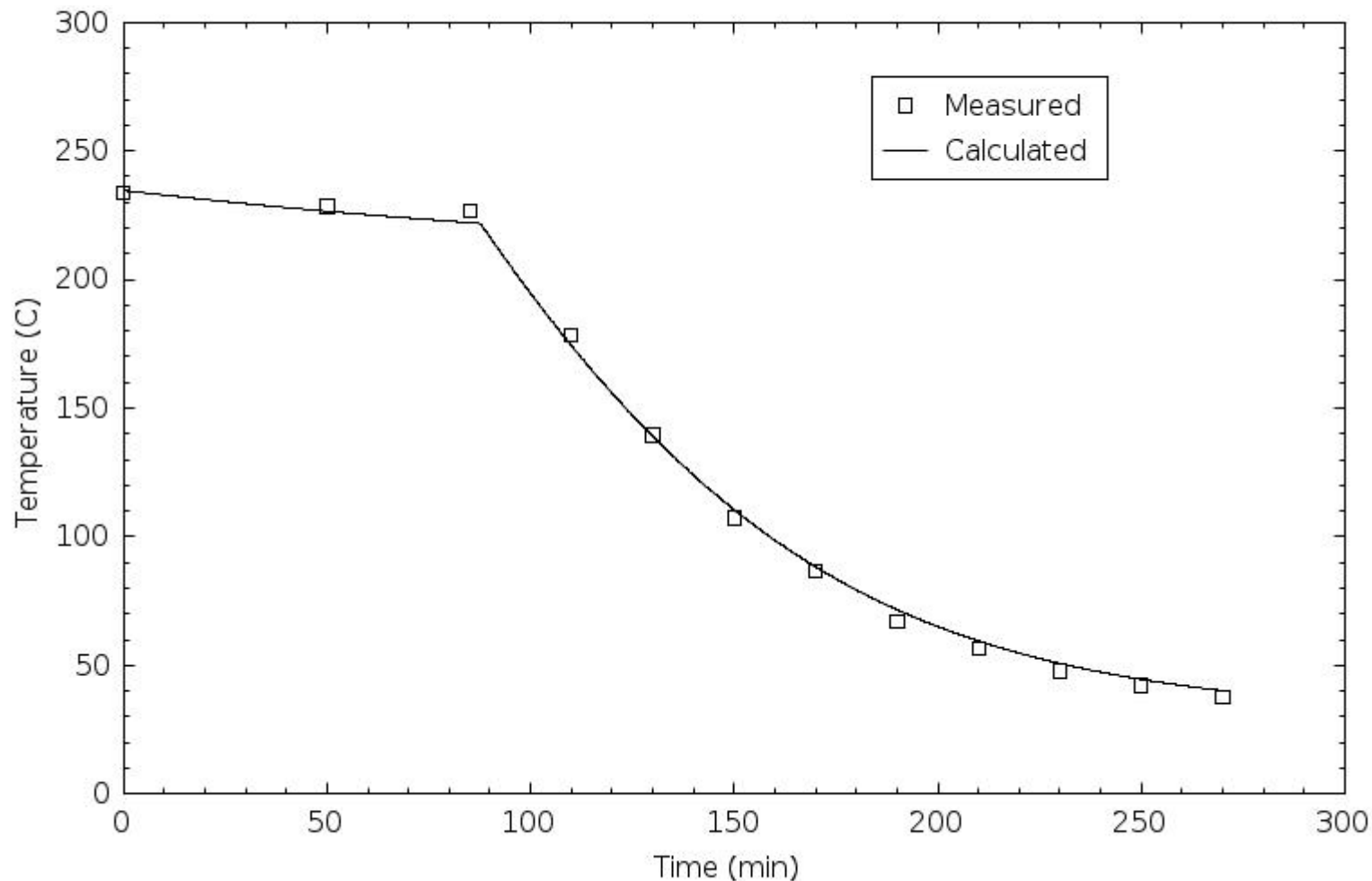
# Axial temperature profiles in the historical cooldown test at 110 min



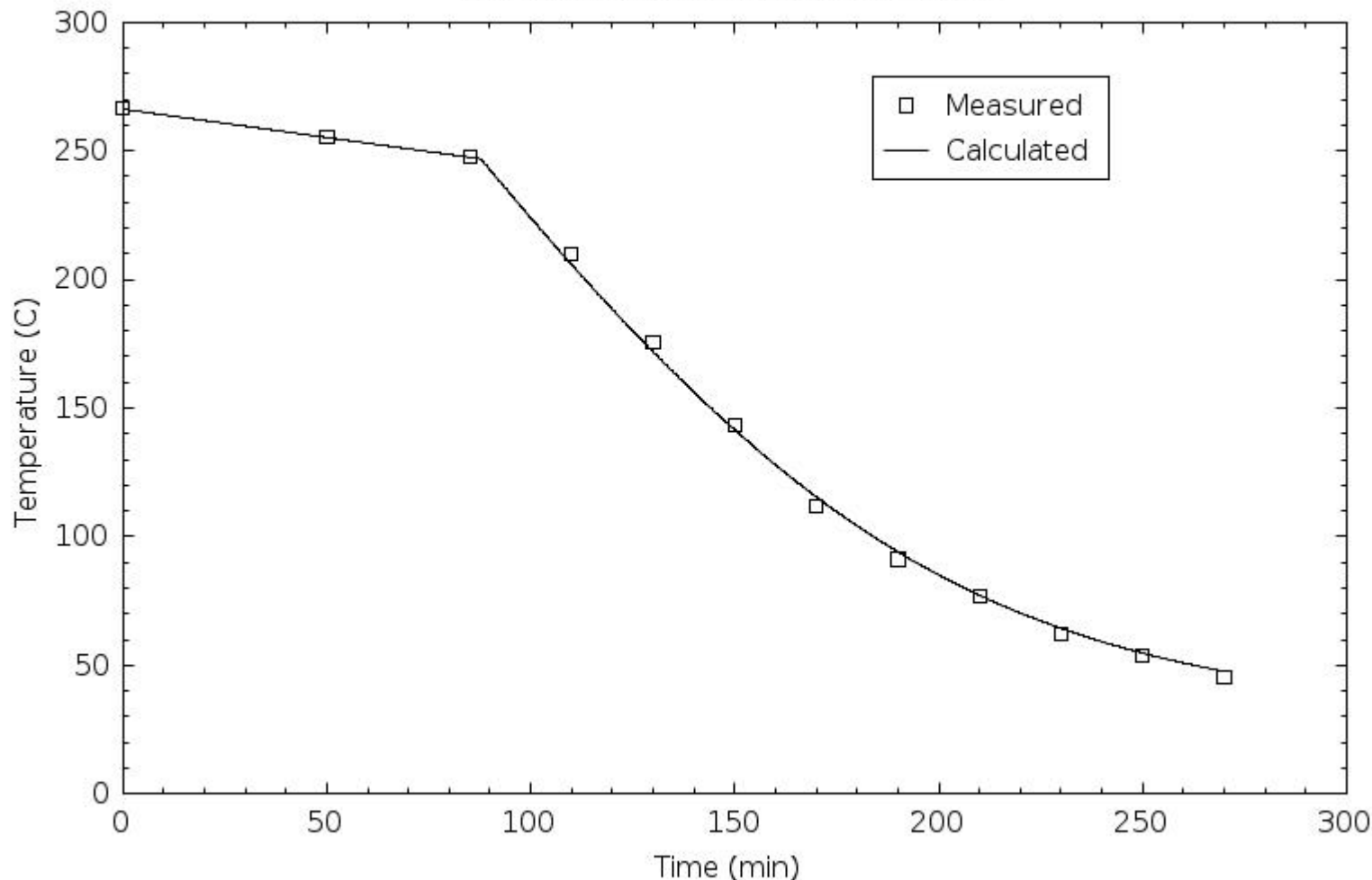
# Axial temperature profiles in the historical cooldown test at 230 min



# Temperature versus time 14 inches from the top of the active fuel in the historical cooldown test

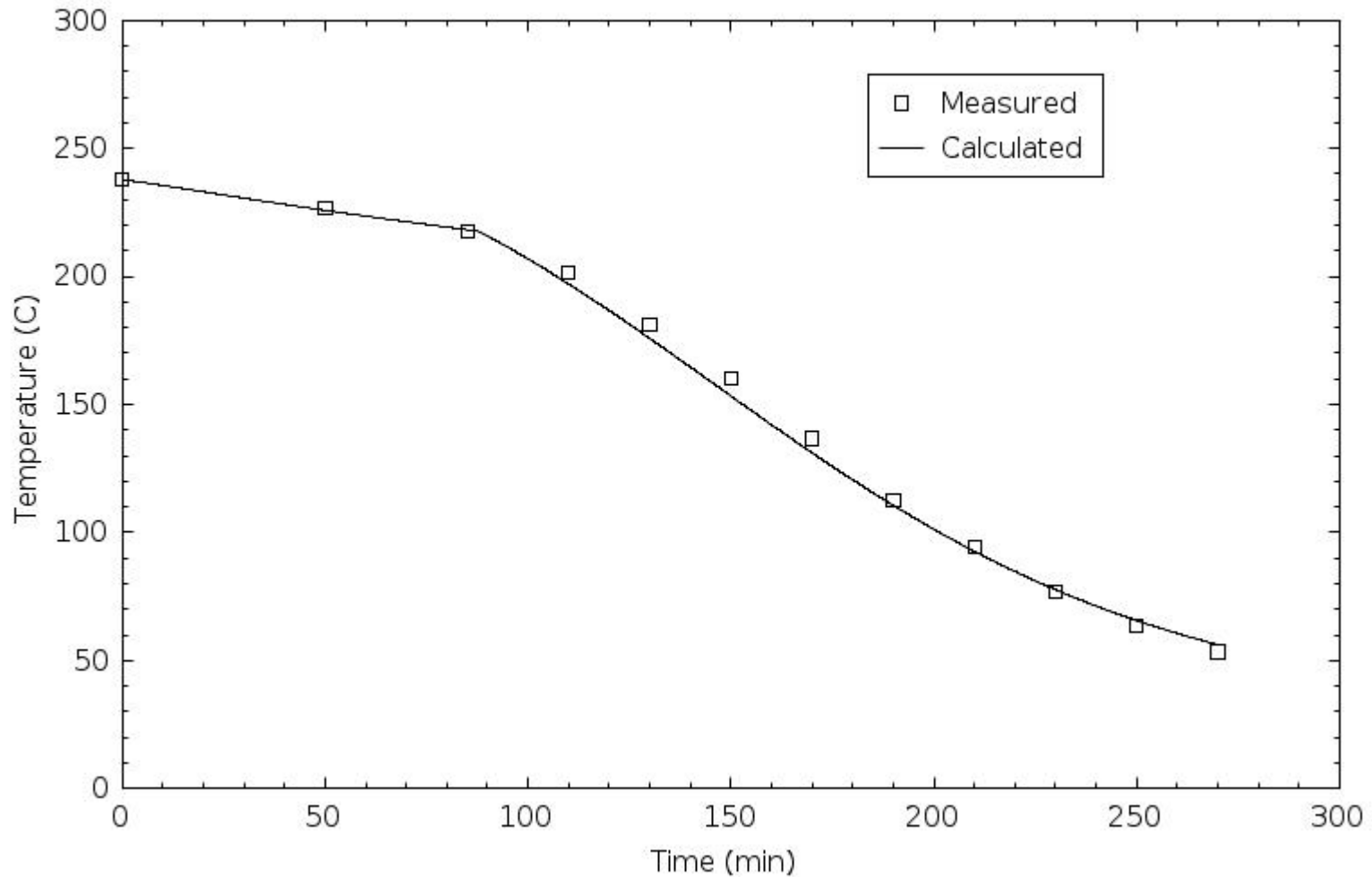


# Temperature versus time 26 inches from the top of the active fuel in the historical cooldown test

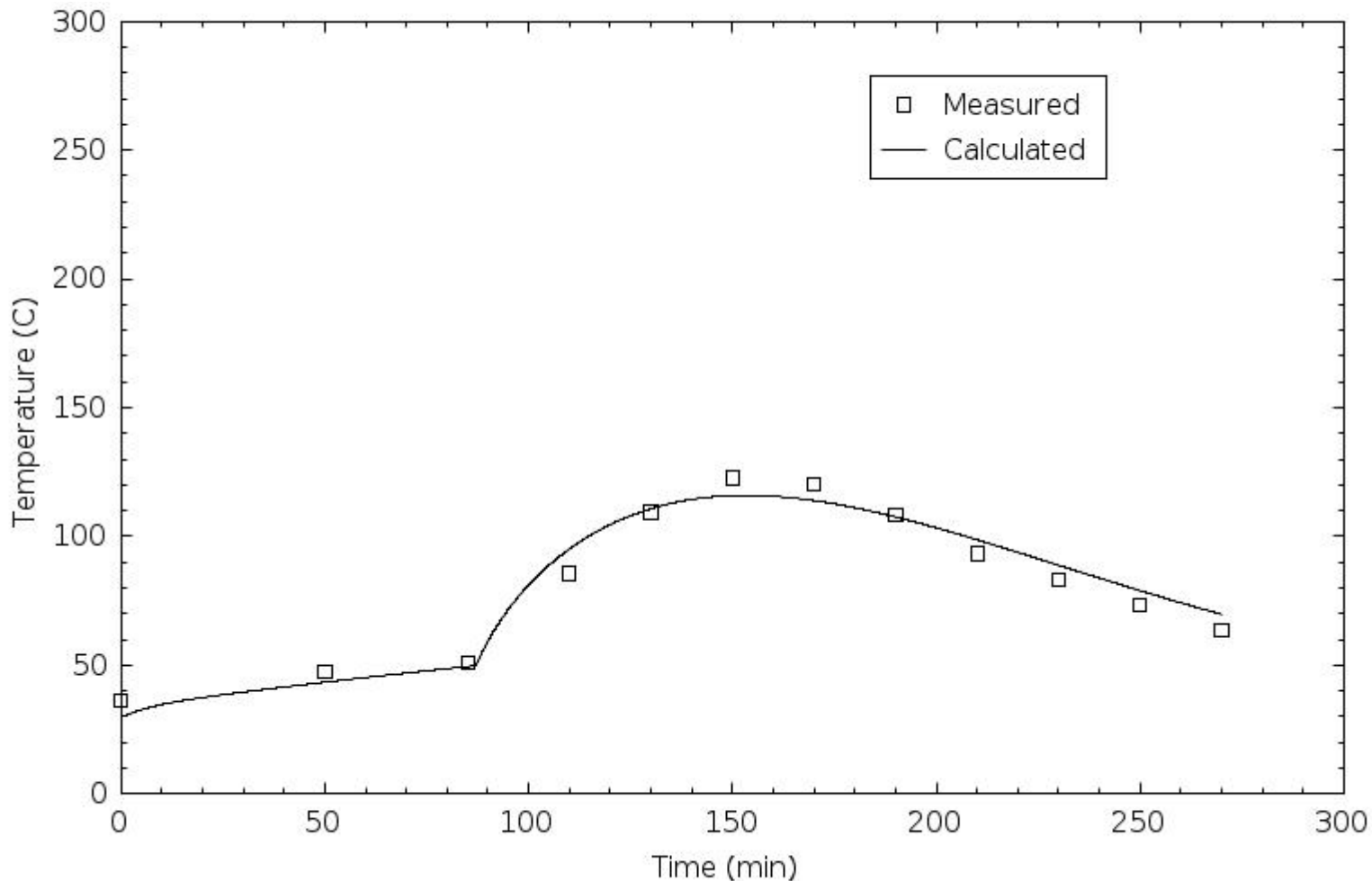




# Temperature versus time 38 inches from the top of the active fuel in the historical cooldown test



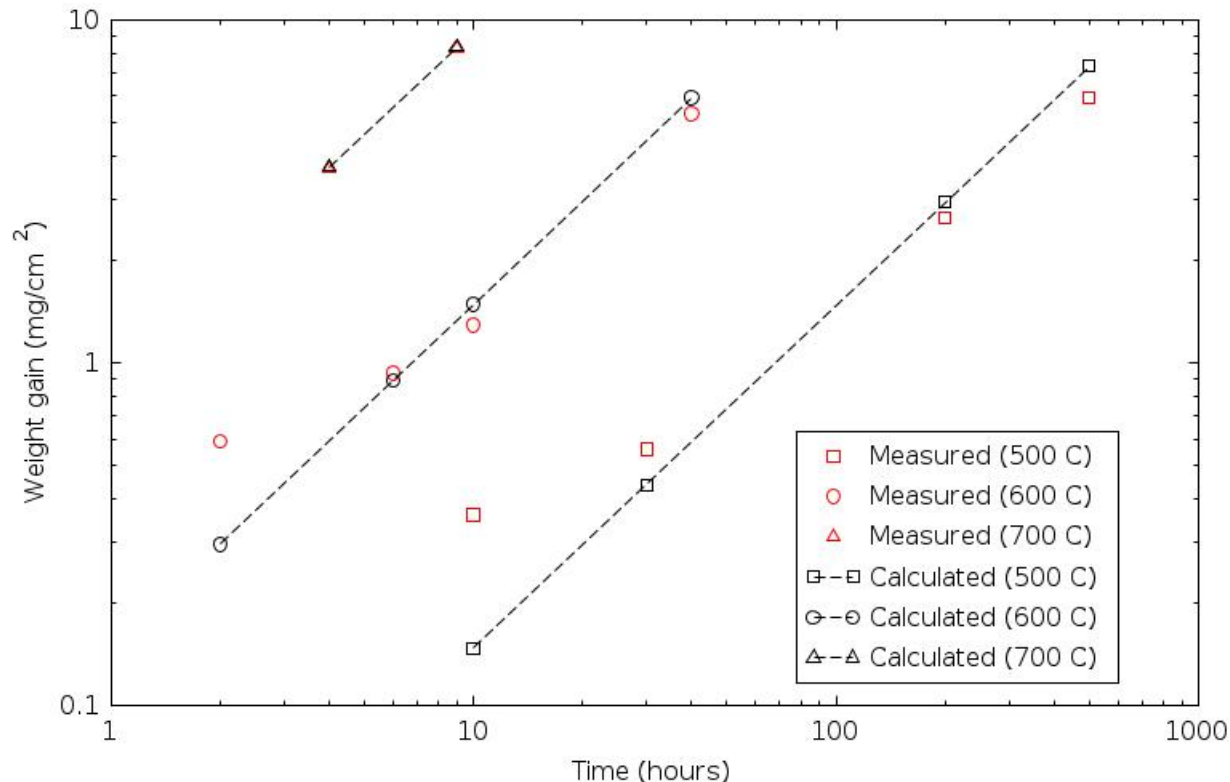
# Temperature versus time 50 inches from the top of the active fuel in the historical cooldown test



## Zircaloy oxidation model

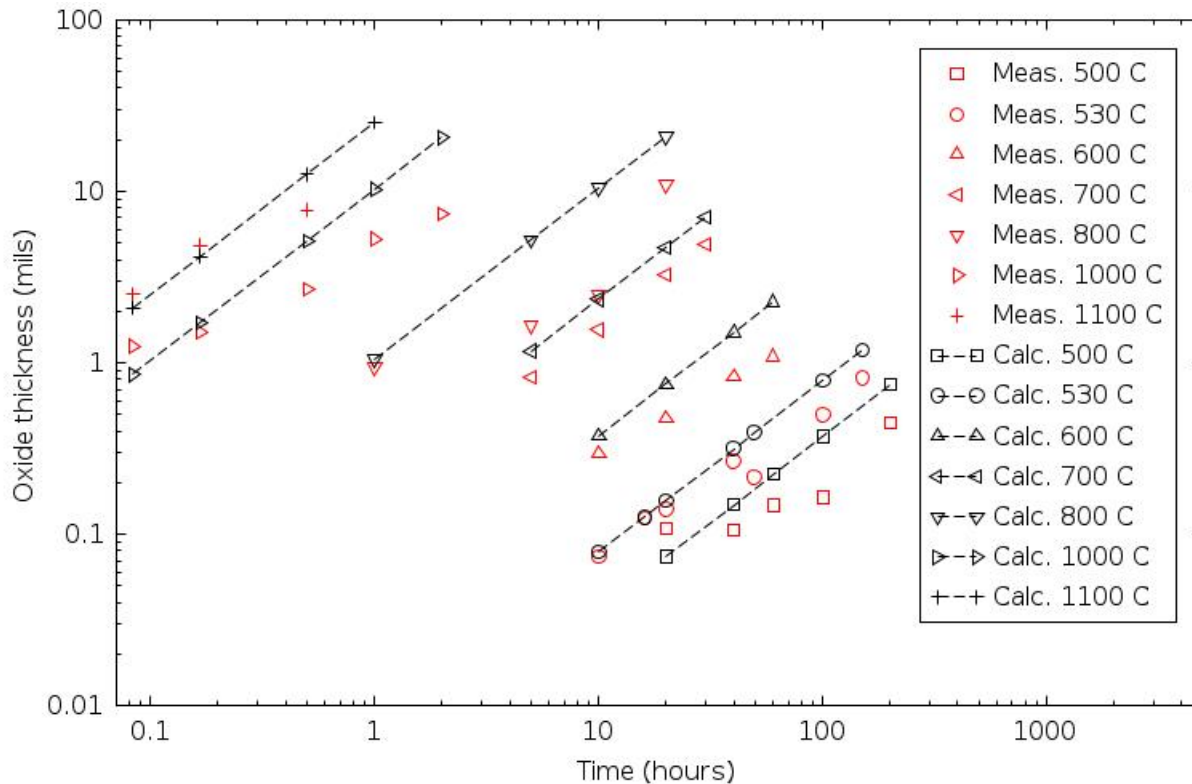
- The oxidation model for TREAT is:
  - $W_{\text{gain}} = A t e^{-Q/(RT)} = 8.5E6 t e^{-3.10E4/(1.9872 T)}$ , where  $W_{\text{gain}}$  is the weight gained due to oxidation (mg/cm<sup>2</sup>),  $t$  is time (hr), and  $T$  is the temperature (K)
  - The model is based on oxidation measurements of Zircaloy-2, which is conservative for TREAT, which has Zircaloy-3
- The RELAP5-3D metal-water reaction model is based on parabolic, not linear, kinetics
- The control system was used to monitor the oxidation of the Zircaloy can at the peak power location

# Oxidation of Zircaloy-2 samples



- Slope changes in measured curves are due to a transition between reaction regimes
- The pre-transition regime was characterized by a reaction rate between parabolic and cubic
- The post-transition regime was linear
- The model is based on the linear, post-transition data

# Oxidation of Zircaloy-3 samples

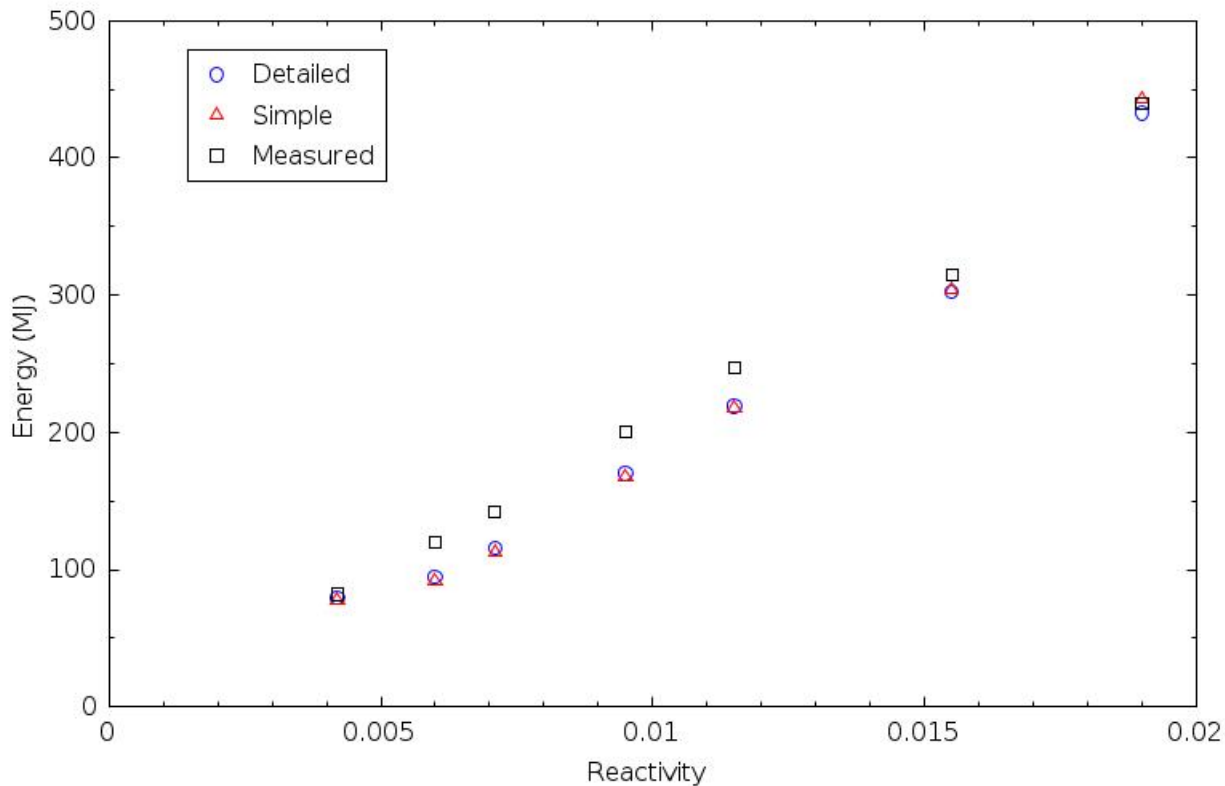


- TREAT fuel assemblies are clad with Zircaloy-3, not Zircaloy-2
- The calculated oxide thickness exceeds the measured value for 24 of 28 points
- Therefore, the model is conservative

## ***Validation results were generated for a wide range of reactivity insertions***

- Seven unshaped experiments conducted around 1960
  - Initiated by near step insertions of reactivity in relatively small cores (~ 150 fuel assemblies)
  - Reactivity insertion varied from 0.42 to 1.90% (0.58 to 2.65\$)
- Two experiments conducted during the early 1990's with the M8 half-slotted core (338 fuel assemblies)
  - Test 2857
    - Unshaped transient initiated by a near step insertion of reactivity (3.85% or 5.36\$)
  - Test 2871
    - Shaped transient with a total reactivity insertion of about 6% or 8.4\$
- Results were similar to those obtained previously with the simple model

# Both models produced a reasonable representation of the historical data



- The energy deposition in was 11% low, on average, with the detailed model
- The calculated results with the detailed model were generally a little better than those obtained previously with the simple model

## Conclusions

- The detailed RELAP5-3D model was validated using data from cooldown, oxidation, and reactivity insertion experiments
- Adjustments were made to the detailed model to match measured cooldown data
  - The axial thermal conductivities of the fuel and insulators were adjusted to match measured core temperatures prior to blower operation
  - The convective heat transfer coefficients were lowered to match measured cooldown rates when the blowers were operating
  - After these adjustments, the quantitative agreement between the calculated and measured temperatures is reasonably good
  - The model captures all of the significant trends observed in the test



## ***Conclusions (cont'd)***

- The RELAP5-3D model monitors the oxidation of the Zircaloy can at the peak power location in the hot fuel element
  - The model is based on oxidation measurements of Zircaloy-2 samples in the post-transition regime
  - The model was validated for TREAT applications using oxidation data from Zircaloy-3 samples
  - The calculated oxide thickness exceeded the measured value for 28 of the 32 data points
  - Therefore, the model is conservative with respect to the calculation of oxidation of the TREAT cladding

## ***Conclusions (cont'd)***

- The detailed model generates results that are in reasonable agreement with measured values of maximum core power, energy deposition, and maximum fuel temperature for a wide range of reactivity insertions
- The detailed and simple models produce similar results for the reactivity insertion experiments
  - Since the simple model runs much faster, it is more suitable for programmatic analyses to support experiments
  - The detailed model is better suited to simulate the long-term response of the reactor during experiments and accidents
  - Therefore, the detailed model is more suitable for reactor safety calculations